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The Use of Geotextiles for Controlling on The Collapse of Gypseous Soils

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ABSTRACT

 $\mathbf{G}_{\mathrm{VPSEOUS}}$ soil is classified as problematic soil, characterised by its characterized by complicated and erratic behavior, and is mostly found in arid and semi-arid areas of the globe. As for Iraq. Gypseous soils cover about 30-35% of the total area of Iraq, as this type of soil is found in the Western Desert and extends to the southern parts of the country. Gypseous soils are considered strong but susceptible to sudden collapse when wet. To control the collapse of gypsum soils, Geotextiles are among the most popular kind of geosynthetic material used for soil reinforcement. The goal of this study is to determine whether woven geotextiles can improve the ultimate bearing capacity of foundations constructed on gypsum soil. The foundation is built from a strong 10mm thick steel plate measuring 100mm x 100mm. In this study, the depth of the geotextile layer that was placed at depths of (0.1B, 0.2B, 0.4B, 0.8B, B) was determined from the width of the foundation used, the number of layers of the reinforcement material (one layer, two layers, and three layers), and the layer-to-layer vertical spacing. Geotextiles: The geotextiles' breadth was also examined. The trials' findings demonstrated that adding geotextile reinforcement to soil can help it have a higher bearing capacity. and reduce the settlement of the gypsum soil. It was found that placing geotextiles at depths of (0.8B-B) is the best depth chosen, and the results were also revealed. The test showed that using three layers of geotextile gave positive results. Additionally, the test findings demonstrated that the reinforcement's composition had a significant impact on the behavior of the foundation.

Keywords: Gypseous soil, Geotextile, Collapsibility, Square footing, Bearing capacity.

1. INTRODUCTION

When the gypseous soil gets wet, it is thought to be a collapsible soil that experiences volume changes due to a major reorganization of soil particles that does not impact loading **(Nashat, 1990; Nashat et al., 2001; Almurshedi et al., 2020)**. Gypsum, or hydrated calcium sulfate,

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is the mineral salt that makes up gypseous soil. Its chemical formula is CaSO₄.2H₂O. (Nafie, 1989; Saaed and Khorshid, 1989). Gypseous soils are robust when they are dry, damp, or drenched in water; when they are soaked, they become significantly weaker and can cause rapid collapse and soil pressure. When gypseous soils are soaked or submerged in water, they dissolve Calcium sulfate, it attempts to lessen the connections between soil particles by stabilizing them soil particles (Al-Busoda, 2008; Karkush et al., 2020; Karkush et al., **2023**). Many additives can be used to stabilize gypseous soils and improve their behavior, preventing them from collapsing. Examples of these additives include emulsified asphalt, lime, and cement. (Latha and Somwanshi, 2009; AlMurshidi et al., 2020; AlMurshidi and Karkush, 2023; Thajeel et al., 2023). Geotextiles materials have been applied, which are thought to be among the modern methods to improve the geotechnical engineering properties of the soil. Soils with poor engineering qualities can be substituted with treated or well-engineered soils in civil engineering projects. However, when the treated soils are deep, this method is deemed unfeasible (expensive). Many researchers are currently searching for new ways to enhance the geotechnical qualities of soil prior to construction. (Naseri et al., 2016; Changizi and Abdolhosein, 2016). Using physical, mechanical, and chemical procedures, soil treatment, also known as stabilization, increases the soil's durability and resilience to external stresses, hence lowering pressure, swelling limits, and permeability.

(Abood, 1994; Al-busoda and Salman, 2013; Iranpour, 2016; AlMurshidi et al., 2023). Standard stabilizers cement, cement dust, fly ash, rice husk ash, leaf ash, lime, and bitumen are used extensively by researchers and engineers in a variety of sources, and their effects on the geotechnical characteristics of gypseous soils have been examined. (Al-Obydi, 1992; Luo et al., 2012; Salman, 2014; Salman and Hamoudi, 2015; Kalhor et al., 2019).

The current experimental work includes improving the geotechnical properties of gypseous soil using geotextiles such as shear and collapse properties and the bearing capacity of soil. The good effect of additional geotextiles is mainly due to how it is used in the treatment of soils. Some previous studies presented the use of geotextiles in soil improvement, as many geotechnical engineers studied the effect of soil reinforcement with geotextile layers.

(Akinmusuru and Akinbolade, 1999) Studied the effect of the height and number of layers of reinforcement on sandy soil after conducting a set of tests on square foundations with three layers of geotextile and concluded that the ideal depth for the first layer of reinforcement is (0.5B). It has been shown that the interlocking of the geotextile layer depends on the friction between it and the sandy soil.

(Yetimoglu et al., 1999) evaluated the ultimate bearing capacity of rectangular foundations built on sandy soil reinforced with one or more layers of geotextile. They found that the highest bearing value for the soil is at the depth (0.3B), which is considered the best reinforcement depth with one layer. (Gabr et al., 1998) Investigated the stress distribution in sandy soils treated with layers of geotextile, and the results showed that soil reinforcement leads to significant stress relief using plate loading experiments with pressure cells (Sitharam and Sireesh, 2004; Shewnim, 2006; Bushra et al., 2013) carried out model experiments in the lab to assess the bearing capability of circular foundations on a sand basis reinforced with multiple geotextile layers. The ultimate bearing capacity improves with the effect of geotextile materials in controlling the collapse of gypseous soil (layer width, layer depth, and number of layers), and treated some geotechnical properties of gypseous soils in the dry and saturated state.



2. MATERIALS

2.1 Soil Sampling and Properties

The study's gypseous soil sample came from Tikrit University, which is 20 kilometers from Tikrit city (220 kilometers from Baghdad). The sample was collected between 0.5 and 1.5 meters below the surface of the ground, with a gypsum content of roughly 54%. After that, the dirt was brought to the lab and allowed to dry for two days in the open. As indicated in **Table 1**, it was well-broken after drying to create fine soil for a number of physical and chemical testing. The gypseous soil's granular distribution is depicted in **Fig. 1**.

| Properties | Value | Specification | Properties | Value | Specification |
|---|------------------------------------|------------------------|-------------------|------------------------|-----------------------|
| Gs (Specefic gravity) | 2.54 | (ASTM D854, 2010) | pН | 8.01 | |
| Y _{dmax} (Maximum Dry Unit Weight) Ο. Μ.C. (Optimum moisture | 17.6 kN/m ³ 11.8% | (ASTM D698, 2021) | CaCO ₃ | 4.6% | (BS 1377-3, 2018) |
| content)D10 mmEffective Size (Theportion of particleswith diameterssmaller than thisvalue is 10%) | 0.18 | (ASTM D- 422, 2007) | CI- | 0.057 | |
| D30 mm (Effective Size The portion of particles with diameters smaller than this value is 30%) | 0.21 | (ASTM D- 422, 2007) | | mg/L | (BS 1377-3, 2018) |
| D60 mm (Effective Size (The portion of particles with diameterssmalle than this value is 60% | 0.41 | (ASTM D- 422, 2007) | | | |
| Sand, S | 94.4% | (ASTM D- | Gpsum content | 54% | |
| Fines | 5.6% | 422, 2007) | EC | 2.43 μS/cm | (ASTM D1125, 2014) |
| Gravel Soil type | <u>0%</u> SP | (USCS) | ESP CEC | 13% 6.54me/ 100g | (ASTM D7503, 2010) |
| TSS (Total soluble salts) SO ₃ (Total sulphate content) | 78.5% 26.75% | (BS 1377-3, 2018) | Ca S | 49.5% 41.7% | (BS 1377-3, 2018) |
| Fe | 5.35% | | XRD | Quartz, Gy | psum, and Dolomite |

Table 1. Physical and chemical properties of the gypseous soil.





Figure 1. Grain size distribution of gypseous soil sample.

2.2 Geotextile

The physical and mechanical characteristics of the woven geotextile used in this investigation.

 Table 2. Properties of geotextile

| Elongation | Tensile strength | Thickness | Opening Size | Mass / unit area |
|------------|-------------------------|-----------|---------------------|-------------------|
| 13% | 50 kN/m ² | 1.5mm | 80 µm | 200 g/ m ² |

2.3 Physical Model

The setup of the physical model as shown in **Fig. 2** and the instruments









Square foundation

hammer



- 1. Soil container $(600 \times 600 \times 400)$ mm. and loading frame.
- 2. Square foundation plate $(10 \times 10 \times 20)$ mm.
- 3. Mechanical hydraulic jack.
- 4. Movable raining system
- 5. Linear Variable Differential Transformer (LVDT) and Data Logger.

Fig. 3 shows the model's geometry in terms of the height and width of the geotextile layer, where the letter (N) shows the inspection number in terms of the placement of the geotextile layer.



Figure 3. The model's geometry

4. RESULTS AND DISCUSSION

4.1 Load-Settlement Tests Influence of The First Geotextile Layer

The effect of geotextile on the bearing and compressibility of gypseous soils was calculated by performing the load-settlement test. The uniformity test was performed according to the physical model, where the steel container (600×600×400) mm and height of 400 mm was filled with gypseous soil by raining technic. Then we gradually apply the loads (axially load) to the base of the foundation the settlements caused by the axially vertical force, and continue to apply the gradual loads until failure occurs in the foundation or soil.

Ten models were performed on the gypseous soils with different with geotextile layers five models in the dry and five models in soaking conditions at (0.1B, 0.2B, 0.4B, 0.8B, and B).



The loading test was performed at the end of treatment by geotextile for gypseous soil samples. Fig. 4 shows the load-settlement curve of tested soil samples in dry conditions. The loading capacity of footing is considered as the stress at failure condition. These figures show that the loading capacity of square footing increased with the increase of the geotextile layers. The loading capacity of gypseous soils treated with geotextile layers is higher than gypseous soils untreated (the loading capacity is calculated by applied load divided by foundation area). It can be noticed that the soil with a high value of shear strength is more affected by the variation of the moisture content than the soil with a low value of shear strength. Fig. 5 shows the load-settlement curve of the tested gypseous soil samples in soaked conditions. A significant increase in the settlement was noticed when the loads were placed on the foundation, and this means that untreated soil can collapse. After completing the loading test at a stress of 225 kPa, the model was immersed in water by the valve at the bottom of the container, immediately after flooding, the settlement of the untreated gypseous soil started to develop at a rapid rate compared with the treated soil. Fig. 6 shows the time versus settlement of treated gypseous soil samples. Ultimately, the reduction in the settlement was 40-60% after 6 days of soaking.



Figure 4. Applied stress versus settlement of gypseous soil treated with geotextile before soaking.



Figure 5. Applied stress versus settlement of gypseous soil treated with geotextile after soaking.





Figure 6. Time versus settlement of soaked gypseous soil treated with geotextile.

4.2 The Influence of Geotextile Layers Number

As anticipated, the bearing capacity increased as the number of reinforcement layers increased. But when the number of geotextile layers rises, the significance of the additional reinforcement layer falls. **Figs. 7 and 8** show the results of models with one, two, and three layers of geotextiles to the equivalent unreinforced form. **Figs. 9 and 10** show the results of models with two layers at (0.2B and 0.4B) and (0.4B and 0.8B) of geotextiles to the equivalent unreinforced fory and soaked. As shown in the figures, The number of geotextile layers rises with the final bearing capacity.



Figure 7. Stress settlement of the model foundation using one, two, three layers of geotextile (dry condition).





Figure 8. Stress settlement of the model foundation using one, two, three layers of geotextile (soaked condition).



Figure 9. Stress settlement of the model foundation using different two layers one thickness of geotextile (dry condition).



Figure 10. Stress settlement of the model foundation using different two layers one thickness of geotextile (soaked condition).



Figs. 11 and 12 show the stress settlement of the model foundation using two different layers of double thickness of geotextile (dry and soaked condition). It was observed that settlement decreases when using a double layer of geotextile at a specific depth.



Figure 11. Stress settlement of the model foundation using different two layers of geotextile double thickness (dry condition).



Figure 12. Stress settlement of the model foundation using different two layers of geotextile double thickness (soaked condition).

4.3 The Influence of The Geotextile Layer's Width

Figs. 13 and 14 show the optimal width of the geotextile layer (W) for gypseous soils reinforced with a single geotextile layer in both dry and flooded cases. The tensile behavior of geotextiles can greatly reduce the pressure exerted on the soil surface. The optimal reinforcement width indicates that the reinforcement portion within the shear zone below the footing will have efficient tensile strength. To enhance tensile strength, An additional length outside the shear zone is required as an anchor. Thus, the width of the shear zone plus



the anchorage zone on both sides adds up to the ideal reinforcement width. Because of this, the reinforcement needs to be five or six times the base's breadth.



Figure 13. Stress leveling with a single layer of reinforced geotextile of various widths (dry condition).





5. CONCLUSIONS

The main purpose of this research is to use geotextile layers to increase the bearing of gypseous soils and reduce the settlement of shallow foundations.

• In every instance, the bearing capacity of gypseous soils reinforced with geotextiles exceeds that of gypseous soils without reinforcement.



- At depth, the bearing capacity increases (0.8B-B) for the reinforcement with geotextile.
- Settlement is the lowest possible when the geotextile layer is placed at a depth of B or at a depth of 0.8B in both dry and soaked cases.
- As the collapse findings amply illustrated, the compressibility of gypsum soil is much reduced when the number of reinforcement layers in the geotextile of gypseous soils is increased.
- Optimum embedment depth to achieve maximum benefit from the soil's bearing capacity and minimum settlement of about (0.4-0.8) B, even when the reinforcement is wrapped around the edges.

NOMENCLATURE Symbol Definitio

| Symbol | Definition | Symbol | Definition |
|----------|---|---------|------------------------|
| D10 | Effective Size (The portion of particles with | 0.М.С % | Optimum moisture |
| | diameterssmaller than this value is 10%) | | content |
| D30 | Effective Size (The portion of particles with | С | Effective cohesion |
| | diameterssmaller than this value is 30%) | | |
| D60 | Effective Size (The portion of particles with | Ø | The Angle of Internal |
| | diameterssmaller than this value is 60%) | | Friction |
| Gs | Specific gravity | X% | Gypsum content |
| γd | Dry Unit Weight | SO3 % | Total sulphate content |
| γd (max) | Maximum Dry Unit Weight | TSS % | Total soluble salts |
| γd (min) | Minimum Dry Unit Weight | SP-SM | poorly graded sand |

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Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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استعمال المنسوجات الأرضية للسيطرة على انهيارية التربة الجبسية

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الخلاصة

تتميز التربة الجبسية بسلوكها المعقد وغير المنتظم، لذلك تصنف من التربة الإشكالية، والتي تتركز بشكل رئيسي في المناطق القاحلة وشبه القاحلة من العالم. أما في العراق فتغطي الترب الجبسية حوالي % (35 – 30) من المساحة الكلية للعراق، حيث يتواجد هذا النوع من التربة في الصحراء الغربية ويمتد إلى الأجزاء الجنوبية من البلاد. تعتبر التربة الجبسية من التربة القوية إلا أنها معرضة للانهيار المفاجئ عند البلل. للتحكم في انهيار التربة الجبسية، فإن أحد أكثر أنواع الأقمشة الأرضية شيوعًا أنها معرضة للانهيار المفاجئ عند البلل. للتحكم في انهيار التربة الجبسية، فإن أحد أكثر أنواع الأقمشة الأرضية شيوعًا المستخدمة لتقوية النابية المواجئ عند البلل. للتحكم في انهيار التربة الجبسية، فإن أحد أكثر أنواع الأقمشة الأرضية شيوعًا المستخدمة لتقوية التربة هي المنسوجات الأرضية. تختبر هذه الدراسة الفوائد المحتملة للتكسية الأرضية المسوجة في زيادة قدرة الحمل النهائية للأساسات المبنية على التربة الجبسية. تم بناء الأساس من لوح فولاذي قوي بسمك 10 مم بقياس 100 مم × المستخدم النهائية للأساسات المبنية على التربة الجبسية. تم بناء الأساس من لوح فولاذي قوي بسمك 10 مم بقياس 100 مم × المن عرض الأساس المستخدم، وعدد طبقات مادة التكسية الأرضية التي تم وضعها على أعماق إلى ما من لوح فولاذي قوي بسمك 10 مم بقياس 100 مم × المن عرض الأساس المستخدم، وعدد طبقات مادة التسليح (طبقة واحدة، طبقتين وثلاث طبقات) والتباعد العمودي بين طبقات (8 من عرض الأساس المستخدم، وعدد طبقات مادة التسليح (طبقة واحدة، طبقتين وثلاث طبقات) والتباعد العمودي بين طبقات 100 مم. تم في هذه الدراسة تحديد عمق طبقة التكسية الأرضية التي تم وضعها على أعماق (, 380 مع) والتباعد العمودي بين طبقات مادة التكسية الأرضية التي تر وضع التربق البقات) والتباعد العمودي بين طبقات (8 من عرض الأساس المستخدم، وعدد طبقات مادة التسليح (طبقة واحدة، طبقتين وثلاث طبقات) والتباعد العمودي بين طبقات مادة الركسية الأرضيية. أظهرت نتائج التحارب أن التربية على أعماق (–888) وعضي ألأرضية الأرضية الأرضية الأرضية الأرضية الأرضية الأرضية الأرضية الأرضية الألموت نتائع الأرضية الرضية، خولي فري وضع التكسية الأرضية مادي معلى نائوي أل مالمان (-880 معاق المام مال الأوضية كشفت نتائج الاختبار أن استخدام ثلاث طبقات من النسيج الأرضي يمال الأوماق المختا

الكلمات المفتاحية: التربة الجبسية، الجيوتكستيل، قابلية الانهيار، القاعدة المربعة، قدرة التحمل، الانضغاطية.